## High Power Differential Line Driver

The EL1503A ADSL Line Driver contains two wideband high-voltage drivers which are ideally suited for both ADSL and HDSL2 applications. They can supply a $39.2 \mathrm{~V}_{\text {P-P }}$ signal into a $22 \Omega$ load while exhibiting very low distortion. The EL1503A also has a number of power saving features. The I $_{\text {ADJ }}$ pin can be used to set the maximum supply current and the $C_{0}$ and $C_{1}$ pins can be used to digitally vary the supply current to one of four modes. These modes include full power, low power, terminate only and power down.

The EL1503A uses current-feedback type amplifiers, which achieve a high slew rate while consuming moderate power. They retain their frequency response over a wide range of externally set gains. The EL1503A operates on $\pm 5 \mathrm{~V}$ to $\pm 12 \mathrm{~V}$ supplies and consumes only 12.5 mA per amplifier.

The device is supplied in a thermally-enhanced 20 Ld SOIC ( 0.300 ") and the small footprint ( $4 \times 5 \mathrm{~mm}$ ) 24 Ld QFN packages. Center pins on each side of the 20 Ld and 16 Ld packages are used as ground connections and heat spreaders. The QFN package has the potential for a low $\theta_{J A}$ ( $<40^{\circ} \mathrm{C} / \mathrm{W}$ ) and dissipates heat by means of a thermal pad that is soldered onto the PCB. All package options are specified for operation over the full $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ temperature range.

## Pinouts



## Features

- High power ADSL driver
- $39.2 \mathrm{~V}_{\text {P-P }}$ differential output drive into $22 \Omega$
- $42.4 \mathrm{~V}_{\mathrm{P}-\mathrm{P}}$ differential output drive into $65 \Omega$
- Driver $2^{\text {nd }} / 3^{r d}$ harmonics of $-66 \mathrm{dBc} /-72 \mathrm{dBc}$ at $2 \mathrm{~V}_{\mathrm{P}-\mathrm{P}}$ into $100 \Omega$ differential
- Supply current of 12.5 mA per amplifier
- Supply current control
- Power saving modes
- Standard surface-mount packages
- Ultra-small QFN package
- Pb-free plus anneal available (RoHS compliant)


## Applications

- ADSL line drivers
- HDSL2 line drivers
- Video distribution amplifiers


## Ordering Information

| PART NUMBER | PART MARKING | TAPE \& REEL | PACKAGE | PKG. DWG. \# |
| :--- | :--- | :---: | :--- | :--- |
| EL1503ACM | EL1503ACM | - | 20 Ld SOIC (0.300") | MDP0027 |
| EL1503ACM-T13 | EL1503ACM | $13^{\prime \prime}$ | 20 Ld SOIC (0.300") | MDP0027 |
| EL1503ACMZ (See Note) | EL1503ACMZ | - | 20 Ld SOIC (0.300") (Pb-Free) | MDP0027 |
| EL1503ACMZ-T13 (See Note) | EL1503ACMZ | $13^{\prime \prime}$ | 20 Ld SOIC (0.300") (Pb-Free) | MDP0027 |
| EL1503ACL | $1503 A C L$ | - | 24 Ld QFN | MDP0046 |
| EL1503ACL-T7 | $1503 A C L$ | $7 "$ | 24 Ld QFN | MDP0046 |
| EL1503ACL-T13 | $1503 A C L$ | $13 "$ | 24 Ld QFN | MDP0046 |
| EL1503ACLZ (See Note) | $1503 A C L Z ~$ | - | 24 Ld QFN (Pb-Free) | MDP0046 |
| EL1503ACLZ-T7 (See Note) | $1503 A C L Z ~$ | 24 Ld QFN (Pb-Free) | MDP0046 |  |
| EL1503ACLZ-T13 (See Note) | $1503 A C L Z ~$ | $13 "$ | 24 Ld QFN (Pb-Free) | MDP0046 |

NOTE: Intersil Pb-free plus anneal products employ special Pb-free material sets; molding compounds/die attach materials and 100\% matte tin plate termination finish, which are RoHS compliant and compatible with both SnPb and Pb-free soldering operations. Intersil Pb-free products are MSL classified at Pb-free peak reflow temperatures that meet or exceed the Pb-free requirements of IPC/JEDEC J STD-020.

```
Absolute Maximum Ratings \(\left(\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}\right.\) )
\(\mathrm{V}_{\mathrm{S}^{+}}\)to \(\mathrm{V}_{\mathrm{S}^{-}}\)Supply Voltage. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 28 V
\(\mathrm{V}_{\mathrm{S}^{+}}\)Voltage to Ground . . . . . . . . . . . . . . . . . . . . . . . . . . 0.3 C to +28 V
\(\mathrm{V}_{\mathrm{S}}\) - Voltage to Ground . . . . . . . . . . . . . . . . . . . . . . . . . . . . 28 V to 0.3 V
Input \(\mathrm{C}_{0} / \mathrm{C}_{1}\) to Ground. . . . . . . . . . . . . . . . . . . . . . . . . . . . . 0.3 V to +7 V
Driver \(\mathrm{V}_{\mathrm{IN}^{+}}\)Voltage . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . \(\mathrm{V}_{\mathrm{S}^{-}}\)to \(\mathrm{V}_{\mathrm{S}^{+}}\)
```

Current into any Input . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 8mA
Output Current from Driver (static) . . . . . . . . . . . . . . . . . . . . 100mA
Operating Temperature Range . . . . . . . . . . . . . . . . $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
Storage Temperature Range . . . . . . . . . . . . . . . . . . $-60^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Operating Junction Temperature . . . . . . . . . . . . . . . $-40^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Power Dissipation . . . . . . . . . . . . . . . . . . . . . . . . . . . . See Curves

CAUTION: Stresses above those listed in "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress only rating and operation of the device at these or any other conditions above those indicated in the operational sections of this specification is not implied.

IMPORTANT NOTE: All parameters having Min/Max specifications are guaranteed. Typical values are for information purposes only. Unless otherwise noted, all tests are at the specified temperature and are pulsed tests, therefore: $T_{J}=T_{C}=T_{A}$

Electrical Specifications $\quad \mathrm{V}_{\mathrm{S}}= \pm 12 \mathrm{~V}, \mathrm{R}_{\mathrm{F}}=1.5 \mathrm{k} \Omega, \mathrm{R}_{\mathrm{L}}=65 \Omega, \mathrm{I}_{\mathrm{ADJ}}=\mathrm{C}_{0}=\mathrm{C}_{1}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$. Amplifiers tested separately.

| PARAMETER | DESCRIPTION | CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SUPPLY CHARACTERISTICS |  |  |  |  |  |  |
| $\mathrm{I}^{+}$(Full Power) | Positive Supply Current per Amplifier | All outputs at $0 \mathrm{~V}, \mathrm{C}_{0}=\mathrm{C}_{1}=0 \mathrm{~V}$ | 10 | 12.5 | 16 | mA |
| Is-(Full Power) | Negative Supply Current per Amplifier | All outputs at $0 \mathrm{~V}, \mathrm{C}_{0}=\mathrm{C}_{1}=0 \mathrm{~V}$ | -15 | -11.5 | -9 | mA |
| $\mathrm{I}^{+}{ }^{+}$(Low Power) | Positive Supply Current per Amplifier | All outputs at $0 \mathrm{~V}, \mathrm{C}_{0}=5 \mathrm{~V}, \mathrm{C}_{1}=0 \mathrm{~V}$ | 7 | 9 | 11.5 | mA |
| $\mathrm{I}^{-}$(Low Power) | Negative Supply Current per Amplifier | All outputs at $0 \mathrm{~V}, \mathrm{C}_{0}=5 \mathrm{~V}, \mathrm{C}_{1}=0 \mathrm{~V}$ | -10.5 | -8 | -6 | mA |
| $\mathrm{I}^{+}$(Terminate) | Positive Supply Current per Amplifier | All outputs at $0 \mathrm{~V}, \mathrm{C}_{0}=0 \mathrm{~V}, \mathrm{C}_{1}=5 \mathrm{~V}$ | 4 | 5.1 | 7 | mA |
| Is-(Terminate) | Negative Supply Current per Amplifier | All outputs at $0 \mathrm{~V}, \mathrm{C}_{0}=0 \mathrm{~V}, \mathrm{C}_{1}=5 \mathrm{~V}$ | -6 | -4 | -3 | mA |
| $\mathrm{I}^{+}$(Power Down) | Positive Supply Current per Amplifier | All outputs at $0 \mathrm{~V}, \mathrm{C}_{0}=\mathrm{C}_{1}=5 \mathrm{~V}$ | 0.75 | 1.05 | 1.7 | mA |
| IS-(Power Down) | Negative Supply Current per Amplifier | All outputs at $0 \mathrm{~V}, \mathrm{C}_{0}=\mathrm{C}_{1}=5 \mathrm{~V}$ | -0.5 | -0.25 | 0.07 | mA |
| $\mathrm{I}_{\text {GND }}$ | GND Supply Current per Amplifier | All outputs at 0 V |  | -1 |  | mA |

## INPUT CHARACTERISTICS

| VOS | Input Offset Voltage |  | -30 |  | 30 | mV |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\Delta \mathrm{V}_{\text {OS }}$ | $V_{\text {OS }}$ Mismatch |  | -15 |  | 15 | mV |
| $\mathrm{I}_{\mathrm{B}}{ }^{+}$ | Non-Inverting Input Bias Current |  | -15 |  | 15 | $\mu \mathrm{A}$ |
| $\mathrm{I}_{\mathrm{B}}{ }^{-}$ | Inverting Input Bias Current |  | -50 |  | 50 | $\mu \mathrm{A}$ |
| $\Delta \mathrm{I}_{\mathrm{B}^{-}}$ | $\mathrm{I}_{\mathrm{B}}$ - Mismatch |  | -30 |  | 30 | $\mu \mathrm{A}$ |
| $\mathrm{R}_{\mathrm{OL}}$ | Transimpedance |  | 0.4 | 0.8 |  | $\mathrm{M} \Omega$ |
| $\mathrm{e}_{\mathrm{N}}$ | Input Noise Voltage |  |  | 3.5 |  | $\mathrm{nV} / \sqrt{\mathrm{Hz}}$ |
| ${ }^{\mathrm{i}} \mathrm{N}$ | -Input Noise Current |  |  | 13 |  | $\mathrm{pA} / \sqrt{\mathrm{Hz}}$ |
| $\mathrm{V}_{\mathrm{IH}}$ | Input High Voltage | $\mathrm{C}_{0} \& \mathrm{C}_{1}$ inputs | 2.7 |  |  | V |
| $\mathrm{V}_{\text {IL }}$ | Input Low Voltage | $\mathrm{C}_{0} \& \mathrm{C}_{1}$ inputs |  |  | 0.8 | V |
| $\mathrm{I}_{\mathrm{H} 1}$ | Input High Current for $\mathrm{C}_{1}$ | $\mathrm{C}_{1}=5 \mathrm{~V}$ | 1.5 |  | 8 | $\mu \mathrm{A}$ |
| $\mathrm{IIHO}^{\text {I }}$ | Input High Current for $\mathrm{C}_{0}$ | $\mathrm{C}_{0}=5 \mathrm{~V}$ | 0.75 |  | 4 | $\mu \mathrm{A}$ |
| IIL | Input Low Current for $\mathrm{C}_{1}$ or $\mathrm{C}_{0}$ | $\mathrm{C}_{1}=0 \mathrm{~V}, \mathrm{C}_{0}=0 \mathrm{~V}$ | -1 |  | 1 | $\mu \mathrm{A}$ |

## OUTPUT CHARACTERISTICS

| $V_{\text {OUT }}$ | Loaded Output Swing | $\mathrm{R}_{\mathrm{L}}=65 \Omega$ | $\pm 10.3$ | $\pm 10.6$ |  | V |
| :--- | :--- | :--- | :---: | :---: | :---: | :---: |
|  | $\mathrm{R}_{\mathrm{L}}=22 \Omega$ | $\pm 9.3$ | $\pm 9.8$ | V |  |  |
| IOL | Linear Output Current | $\mathrm{A}_{\mathrm{V}}=5, \mathrm{R}_{\mathrm{L}}=10 \Omega, \mathrm{f}=100 \mathrm{kHz}$, <br> $\mathrm{THD}=-60 \mathrm{dBc}$ |  | 450 | mA |  |
| IOUT | Output Current | $\mathrm{V}_{\text {OUT }}=1 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=1 \Omega$ |  | 1 | A |  |

Electrical Specifications $V_{S}= \pm 12 \mathrm{~V}, \mathrm{R}_{\mathrm{F}}=1.5 \mathrm{k} \Omega, \mathrm{R}_{\mathrm{L}}=65 \Omega, \mathrm{I}_{\mathrm{ADJ}}=\mathrm{C}_{0}=\mathrm{C}_{1}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$. Amplifiers tested separately. (Continued)

| PARAMETER | DESCRIPTION | CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DYNAMIC PERFORMANCE |  |  |  |  |  |  |
| BW | -3dB Bandwidth | $A_{V}=+5$ |  | 80 |  | MHz |
| HD2 | 2nd Harmonic Distortion | $\mathrm{f}_{\mathrm{C}}=1 \mathrm{MHz}, \mathrm{R}_{\mathrm{L}}=100 \Omega, \mathrm{~V}_{\text {OUT }}=2 \mathrm{~V}_{\mathrm{P}-\mathrm{P}}$ |  | -76 |  | dBc |
|  |  | $\mathrm{f}_{\mathrm{C}}=1 \mathrm{MHz}, \mathrm{R}_{\mathrm{L}}=25 \Omega, \mathrm{~V}_{\text {OUT }}=2 \mathrm{~V}_{\mathrm{P}-\mathrm{P}}$ |  | -72 |  | dBc |
| HD3 | 3rd Harmonic Distortion | $\mathrm{f}_{\mathrm{C}}=1 \mathrm{MHz}, \mathrm{R}_{\mathrm{L}}=100 \Omega, \mathrm{~V}_{\text {OUT }}=2 \mathrm{~V}_{\mathrm{P}-\mathrm{P}}$ |  | -76 |  | dBc |
|  |  | $\mathrm{f}_{\mathrm{C}}=1 \mathrm{MHz}, \mathrm{R}_{\mathrm{L}}=25 \Omega, \mathrm{~V}_{\text {OUT }}=2 \mathrm{~V}_{\mathrm{P}-\mathrm{P}}$ |  | -72 |  | dBc |
| SR | Slewrate | $\mathrm{V}_{\text {OUT }}$ from -8 V to +8 V Measured at $\pm 4 \mathrm{~V}$ | 700 | 1100 |  | $\mathrm{V} / \mu \mathrm{s}$ |

## Typical Performance Curves



FIGURE 1. DRIVER DIFFERENTIAL FREQUENCY RESPONSE vs RF (FULL POWER MODE)


FIGURE 3. DRIVER DIFFERENTIAL FREQUENCY RESPONSE vs $R_{F}$ (2/3 POWER MODE)


FIGURE 2. DRIVER DIFFERENTIAL FREQUENCY RESPONSE vs $R_{F}$ (FULL POWER MODE)


FIGURE 4. DRIVER DIFFERENTIAL FREQUENCY RESPONSE vs $R_{F}$ (2/3 POWER MODE)

Typical Performance Curves (Continued)


FIGURE 5. DRIVER DIFFERENTIAL FREQUENCY RESPONSE vs $\mathbf{R}_{\mathbf{F}}$ (TERMINATE MODE)


FIGURE 7. DRIVER DIFFERENTIAL FREQUENCY RESPONSE vs $R_{F}$ (FULL POWER MODE)


FIGURE 9. DRIVER DIFFERENTIAL FREQUENCY RESPONSE vs $R_{F}$ (2/3 POWER MODE)


FIGURE 6. DRIVER DIFFERENTIAL FREQUENCY RESPONSE vs $R_{F}$ (TERMINATE MODE)


FIGURE 8. DRIVER DIFFERENTIAL FREQUENCY RESPONSE vs $R_{F}$ (FULL POWER MODE)


FIGURE 10. DRIVER DIFFERENTIAL FREQUENCY RESPONSE vs $R_{F}$ (2/3 POWER MODE)

## Typical Performance Curves (Continued)



FIGURE 11. DRIVER DIFFERENTIAL FREQUENCY RESPONSE vs $R_{F}$ (TERMINATE MODE)


FIGURE 13. DRIVER INPUT VOLTAGE and FEEDBACK CURRENT NOISE vs FREQUENCY


FIGURE 15. POSITIVE SUPPLY REJECTION vs FREQUENCY


FIGURE 12. DRIVER DIFFERENTIAL FREQUENCY RESPONSE vs $R_{F}$ (TERMINATE MODE)


FIGURE 14. SUPPLY CURRENT vs SUPPLY VOLTAGE


FIGURE 16. NEGATIVE SUPPLY REJECTION vs FREQUENCY

Typical Performance Curves (Continued)


FIGURE 17. OUTPUT IMPEDANCE vs FREQUENCY


FIGURE 19. DIFFERENTIAL HARMONIC DISTORTION vs OUTPUT AMPLITUDE (FULL POWER)


FIGURE 21. DIFFERENTIAL HARMONIC DISTORTION vs OUTPUT AMPLITUDE (2/3 POWER)


FIGURE 18. OUTPUT IMPEDANCE vs FREQUENCY


FIGURE 20. DIFFERENTIAL HARMONIC DISTORTION vs OUTPUT AMPLITUDE (FULL POWER)


FIGURE 22. DIFFERENTIAL HARMONIC DISTORTION vs OUTPUT AMPLITUDE

## Typical Performance Curves (Continued)



FIGURE 23. DIFFERENTIAL TOTAL HARMONIC DISTORTION vs OUTPUT AMPLITUDE


FIGURE 25. DIFFERENTIAL HARMONIC DISTORTION vs OUTPUT AMPLITUDE (FULL POWER)


FIGURE 27. DIFFERENTIAL HARMONIC DISTORTION vs OUTPUT AMPLITUDE (2/3 POWER)


FIGURE 24. DIFFERENTIAL TOTAL HARMONIC DISTORTION vs OUTPUT AMPLITUDE


FIGURE 26. DIFFERENTIAL HARMONIC DISTORTION vs OUTPUT AMPLITUDE (FULL POWER)


FIGURE 28. DIFFERENTIAL HARMONIC DISTORTION vs OUTPUT AMPLITUDE (2/3 POWER)

Typical Performance Curves (Continued)


FIGURE 29. DIFFERENTIAL TOTAL HARMONIC DISTORTION vs OUTPUT AMPLITUDE


FIGURE 31. DIFFERENTIAL BANDWIDTH vs SUPPLY VOLTAGE


FIGURE 33. Is vs RSET


FIGURE 30. DIFFERENTIAL TOTAL HARMONIC DISTORTION vs OUTPUT AMPLITUDE


FIGURE 32. DIFFERENTIAL PEAKING vs SUPPLY VOLTAGE


FIGURE 34. Is vs RET

## Typical Performance Curves (Continued)



FIGURE 35. IS vS ISET


FIGURE 37. POWER DISSIPATION vS AMBIENT TEMPERATURE for VARIOUS MOUNTED $\theta_{\text {JAS }}$


FIGURE 36. Is vs ISET


FIGURE 38. POWER DISSIPATION vs AMBIENT TEMPERATURE

## Test Circuit




## Pin Descriptions

| $\begin{gathered} 20 \text { Ld SOIC } \\ \left(0.300{ }^{\prime \prime}\right) \end{gathered}$ | 24 Ld QFN | PIN NAME | FUNCTION | CIRCUIT |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 23 | $\mathrm{V}_{\text {IN }}$ - A | Channel A Inverting Input |  |
| 2 | 24 | V OUTA | Channel A Output | (Reference Circuit 1) |
| 3 | 3 | $\mathrm{V}_{\mathrm{S}^{-}}$ | Negative Supply |  |
| 4, 5, 6, 7 | 7 | GND | Ground Connection |  |
| 8 | 8 | $\mathrm{V}_{\text {IN }}+\mathrm{A}$ | Channel A Non-Inverting Input | CIRCUIT 2 |
| 9 | 9 | $\mathrm{C}_{1}$ | Current Control Bit 1 | CIRCUIT 3 |
| 10 | 10 | $\mathrm{C}_{0}$ | Current Control Bit 0 | (Reference Circuit 3) |
| 11 | $\begin{gathered} 1,2,4,5,6,14 \\ 15,16,18,19 \\ 22 \end{gathered}$ | NC | Not Connected |  |
| 12 | 11 | ${ }^{\text {IADJ }}$ | Supply Current Control Pin |  |
| 13 | 12 | $\mathrm{V}_{\text {IN }}+\mathrm{B}$ | Channel B Non-Inverting Input | (Reference Circuit 2) |
| 14, 15, 16, 17 | 13 | GND | Ground Connection |  |
| 18 | 17 | $\mathrm{V}_{\mathrm{S}^{+}}$ | Positive Supply |  |
| 19 | 20 | $\mathrm{V}_{\text {OUT }}{ }^{\text {B }}$ | Channel B Output | (Reference Circuit 1) |
| 20 | 21 | $\mathrm{V}_{\text {IN }}$ - ${ }^{\text {d }}$ | Channel B Inverting Input | (Reference Circuit 1) |
| - | 7 |  | Reserve for Future Use | Internally Unconnected |

## Applications Information

The EL1503A consists of two high-power line driver amplifiers that can be connected for full duplex differential line transmission. The amplifiers are designed to be used with signals up to 4 MHz and produce low distortion levels. A typical interface circuit is shown in Figure 39 below.


FIGURE 39. TYPICAL LINE INTERFACE CONNECTION
The amplifiers are wired with one in positive gain and the other in a negative gain configuration to generate a differential output for a single-ended input. They will exhibit very similar frequency responses for gains of three or greater and thus generate very small common-mode outputs over frequency, but for low gains the two drivers $R_{F}$ 's need to be adjusted to give similar frequency responses. The positive-gain driver will generally exhibit more bandwidth and peaking than the negative-gain driver.
If a differential signal is available to the drive amplifiers, they may be wired so:


FIGURE 40. DRIVERS WIRED FOR DIFFERENTIAL INPUT
Each amplifier has identical positive gain connections, and optimum common-mode rejection occurs. Further, DC input errors are duplicated and create common-mode rather than differential line errors.

## Input Connections

The EL1503A amplifiers are somewhat sensitive to source impedance. In particular, they do not like being driven by inductive sources. More than 100 nH of source impedance
can cause ringing or even oscillations. This inductance is equivalent to about 4" of unshielded wiring, or 6" of unterminated transmission line. Normal high-frequency construction obviates any such problem.

## Power Supplies \& Dissipation

Due to the high power drive capability of the EL1503A, much attention needs to be paid to power dissipation. The power that needs to be dissipated in the EL1503A has two main contributors. The first is the quiescent current dissipation. The second is the dissipation of the output stage.

The quiescent power in the EL1503A is not constant with varying outputs. In reality, 7 mA of the 12.5 mA needed to power each driver is converted in to output current. Therefore, in the equation below we should subtract the average output current, $I_{0}$, or 7 mA , whichever is the lowest. We'll call this term $\mathrm{I}_{\mathrm{X}}$.
Therefore, we can determine a quiescent current with the equation:
$P_{\text {Dquiescent }}=V_{S} \times\left(I_{S}-2 I_{X}\right)$
where:

$$
\begin{aligned}
& V_{S} \text { is the supply voltage }\left(V_{S^{+}} \text {to } V_{S^{-}}\right) \\
& I_{S} \text { is the maximum quiescent supply current }\left(I_{S^{+}}+I_{S^{-}}\right) \\
& \left.I_{X} \text { is the lesser of } I_{O} \text { or } 7 \mathrm{~mA} \text { (generally } I_{X}=7 \mathrm{~mA}\right)
\end{aligned}
$$

The dissipation in the output stage has two main contributors. Firstly, we have the average voltage drop across the output transistor and secondly, the average output current. For minimal power dissipation, the user should select the supply voltage and the line transformer ratio accordingly. The supply voltage should be kept as low as possible, while the transformer ratio should be selected so that the peak voltage required from the EL1503A is close to the maximum available output swing. There is a trade of however with the selection of transformer ratio. As the ratio is increased, the receive signal available to the receivers is reduced.

Once the user has selected the transformer ratio, the dissipation in the output stages can be selected with the following equation:
$\mathrm{P}_{\text {Dtransistors }}=2 \times \overline{I_{\mathrm{O}}} \times\left(\frac{\mathrm{V}_{\mathrm{S}}}{2}-\overline{\mathrm{V}_{\mathrm{O}}}\right)$
where:
$\mathrm{V}_{\mathrm{S}}$ is the supply voltage $\left(\mathrm{V}_{\mathrm{S}^{+}}\right.$to $\left.\mathrm{V}_{\mathrm{S}^{-}}\right)$
$V_{O}$ is the average output voltage per channel
$I_{O}$ is the average output current per channel
The overall power dissipation ( $\mathrm{P}_{\text {DISS }}$ ) is obtained by adding $P_{\text {Dquiescent }}$ and $\mathrm{P}_{\text {Dtransistor }}$.

Then, the $\theta_{\mathrm{JA}}$ requirement needs to be calculated. This is done using the equation:
$\theta_{J A}=\frac{\left(T_{J U N C T}-T_{A M B}\right)}{P_{\text {DISS }}}$
where:
$\mathrm{T}_{\text {JUNCT }}$ is the maximum die temperature $\left(150^{\circ} \mathrm{C}\right)$
$\mathrm{T}_{\text {AMB }}$ is the maximum ambient temperature
$P_{\text {DISS }}$ is the dissipation calculated above
$\theta_{J A}$ is the junction to ambient thermal resistance for the package when mounted on the PCB
This $\theta_{J A}$ value is then used to calculate the area of copper needed on the board to dissipate the power. The graph below show various $\theta_{\mathrm{JA}}$ for the SO20 mounted on different copper foil areas.


FIGURE 41. THERMAL RESISTANCE of 20 Ld SOIC (0.300") EL1503A vs BOARD COPPER AREA

A separate application note details the 24 Ld QFN PCB design considerations.

## Single Supply Operation

The EL1503A can also be powered from a single supply voltage. When operating in this mode, the GND pins can still be connected directly to GND. To calculate power dissipation, the equations in the previous section should be used, with $\mathrm{V}_{\mathrm{S}}$ equal to half the supply rail.

## EL1503A PCB Design

A separate application note details the 24 Ld QFN PCB design considerations. The SOIC power packages (20 leads) are designed so that heat may be conducted away from the device in an efficient manner. To disperse this heat, the center leads ( 4 per side for the 20 lead and 2 per side for the 16 lead) are internally connected to the mounting platform of the die. Heat flows through the leads into the circuit board copper, then spreads and convects to air. Thus, the ground plane on the component side of the board becomes the heatsink. This has proven to be a very effective
technique, but several aspects of board layout should be noted. First, the heat should not be shunted to internal copper layers of the board nor backside foil, since the feedthroughs and fiberglass of the board are not very thermally conductive. To obtain the best thermal resistance of the mounted part, $\theta_{\mathrm{JA}}$, the topside copper ground plane should have as much area as possible and be as thick as practical. If possible, the solder mask should be cut away from the EL1503A to improve thermal resistance. Finally, metal heatsinks can be placed against the board close to the part to draw heat toward the chassis.

## Output Loading

While the drive amplifiers can output in excess of 500 mA transiently, the internal metallization is not designed to carry more than 100 mA of steady DC current and there is no current-limit mechanism. This allows safely driving rms sinusoidal currents of $2 \times 100 \mathrm{~mA}$, or 200 mA . This current is more than that required to drive line impedances to large output levels, but output short circuits cannot be tolerated. The series output resistor will usually limit currents to safe values in the event of line shorts. Driving lines with no series resistor is a serious hazard.

The amplifiers are sensitive to capacitive loading. More than 25 pF will cause peaking of the frequency response. The same is true of badly terminated lines connected without a series matching resistor.

## Power Supplies

The power supplies should be well bypassed close to the EL1503A. A $3.3 \mu \mathrm{~F}$ tantalum capacitor for each supply works well. Since the load currents are differential, they should not travel through the board copper and set up ground loops that can return to amplifier inputs. Due to the class AB output stage design, these currents have heavy harmonic content. If the ground terminal of the positive and negative bypass capacitors are connected to each other directly and then returned to circuit ground, no such ground loops will occur. This scheme is employed in the layout of the EL1503A demonstration board, and documentation can be obtained from the factory.

## Feedback Resistor Value

The bandwidth and peaking of the amplifiers varies with supply voltage somewhat and with gain settings. The feedback resistor values can be adjusted to produce an optimal frequency response. Here is a series of resistor values that produce an optimal driver frequency response (1dB peaking) for different supply voltages and gains:
TABLE 1. OPTIMUM DRIVER FEEDBACK RESISTOR for
VARIOUS GAINS and SUPPLY VOLTAGES

| SUPPLY <br> VOLTAGE | DRIVER VOLTAGE GAIN |  |  |
| :---: | :---: | :---: | :---: |
|  | $\mathbf{2 . 5}$ | $\mathbf{5}$ | $\mathbf{1 0}$ |
| $\pm 5 \mathrm{~V}$ | 2.7 k | 2.2 k | 2.0 k |
| $\pm 12 \mathrm{~V}$ | 2.2 k | 2.0 k | 2.0 k |

## Power Control Function

The EL1503A contains two forms of power control operation. Two digital inputs, $\mathrm{C}_{0}$ and $\mathrm{C}_{1}$, can be used to control the supply current of the EL1503A drive amplifiers. As the supply current is reduced, the EL1503A will start to exhibit slightly higher levels of distortion and the frequency response will be limited. The 4 power modes of the EL1503A are set up as shown in the table 2 .

TABLE 2. POWER MODES of the EL1503A

| $\mathbf{C}_{\mathbf{1}}$ | $\mathbf{C}_{\mathbf{0}}$ | OPERATION |
| :---: | :---: | :--- |
| 0 | 0 | IS $_{\text {S }}$ full power mode (CO or CP ) |
| 0 | 1 | $2 / 3$ I ${ }_{\text {S }}$ power mode (CO or CP ) |
| 1 | 0 | $1 / 3$ I s terminate only mode |
| 1 | 1 | Power down |

Another method for controlling the power consumption of the EL1503A is to connect a resistor from the $\mathrm{I}_{\text {ADJ }}$ pin to ground. When this pin is grounded (the normal state), the supply current per channel is as per the specifications table on page 3. When a resistor is inserted, the supply current is scaled according to the "IS vs $\mathrm{R}_{\mathrm{SET}}$ " graphs on page 10 in the Performance Curves section.

Both methods of power control can be used simultaneously. In this case, positive and negative supply currents (per amp) are given by the equations below:

$$
\begin{aligned}
& \left.\mathrm{I}_{\mathrm{S}^{+}}=1 \mathrm{~mA}+\overline{\left(\mathrm{C}_{1}\right.} \times 2 / 3\right) \times \frac{12.5 \mathrm{~mA}}{\left(1+\mathrm{R}_{\mathrm{SET}} \div 1 \mathrm{k}\right)} \\
& +\overline{\left(\mathrm{C}_{0} \times 1 / 3\right) \times \frac{12.5 \mathrm{~mA}}{\left(1+\mathrm{R}_{\mathrm{SET}} \div 1 \mathrm{k}\right)}} \\
& \left.\mathrm{I}_{\mathrm{S}^{-}}=0+\overline{\left(\mathrm{C}_{1}\right.} \times 2 / 3\right) \times \frac{12.5 \mathrm{~mA}}{\left(1+\mathrm{R}_{\mathrm{SET}} \div 1 \mathrm{k}\right)} \\
& \left.+\overline{\left(\mathrm{C}_{0}\right.} \times 1 / 3\right) \times \frac{12.5 \mathrm{~mA}}{\left(1+\mathrm{R}_{\mathrm{SET}} \div 1 \mathrm{k}\right)}
\end{aligned}
$$

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## Small Outline Package Family (SO)





MDP0027
SMALL OUTLINE PACKAGE FAMILY (SO)

| SYMBOL | INCHES |  |  |  |  |  |  | TOLERANCE | NOTES |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SO-8 | SO-14 | $\begin{gathered} \text { SO16 } \\ (0.150 ") \end{gathered}$ | $\begin{gathered} \text { SO16 (0.300") } \\ \text { (SOL-16) } \end{gathered}$ | $\begin{gathered} \text { SO20 } \\ \text { (SOL-20) } \end{gathered}$ | $\begin{gathered} \text { SO24 } \\ (\mathrm{SOL}-24) \end{gathered}$ | $\begin{gathered} \text { SO28 } \\ \text { (SOL-28) } \end{gathered}$ |  |  |
| A | 0.068 | 0.068 | 0.068 | 0.104 | 0.104 | 0.104 | 0.104 | MAX | - |
| A1 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 | 0.007 | $\pm 0.003$ | - |
| A2 | 0.057 | 0.057 | 0.057 | 0.092 | 0.092 | 0.092 | 0.092 | $\pm 0.002$ | - |
| b | 0.017 | 0.017 | 0.017 | 0.017 | 0.017 | 0.017 | 0.017 | $\pm 0.003$ | - |
| c | 0.009 | 0.009 | 0.009 | 0.011 | 0.011 | 0.011 | 0.011 | $\pm 0.001$ | - |
| D | 0.193 | 0.341 | 0.390 | 0.406 | 0.504 | 0.606 | 0.704 | $\pm 0.004$ | 1,3 |
| E | 0.236 | 0.236 | 0.236 | 0.406 | 0.406 | 0.406 | 0.406 | $\pm 0.008$ | - |
| E1 | 0.154 | 0.154 | 0.154 | 0.295 | 0.295 | 0.295 | 0.295 | $\pm 0.004$ | 2, 3 |
| e | 0.050 | 0.050 | 0.050 | 0.050 | 0.050 | 0.050 | 0.050 | Basic | - |
| L | 0.025 | 0.025 | 0.025 | 0.030 | 0.030 | 0.030 | 0.030 | $\pm 0.009$ | - |
| L1 | 0.041 | 0.041 | 0.041 | 0.056 | 0.056 | 0.056 | 0.056 | Basic | - |
| h | 0.013 | 0.013 | 0.013 | 0.020 | 0.020 | 0.020 | 0.020 | Reference | - |
| N | 8 | 14 | 16 | 16 | 20 | 24 | 28 | Reference | - |

NOTES:
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1. Plastic or metal protrusions of 0.006 " maximum per side are not included.
2. Plastic interlead protrusions of 0.010 " maximum per side are not included.
3. Dimensions "D" and "E1" are measured at Datum Plane "H".
4. Dimensioning and tolerancing per ASME Y14.5M-1994

## QFN (Quad Flat No-Lead) Package Family

(A)


TOP VIEW


BOTTOM VIEW


MDP0046
QFN (QUAD FLAT NO-LEAD) PACKAGE FAMILY
(COMPLIANT TO JEDEC MO-220)

|  | MILLIMETERS |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SYMBOL | QFN44 | QFN3 | QFN32 |  | TOLERANCE | NOTES |
| A | 0.90 | 0.90 | 0.90 | 0.90 | $\pm 0.10$ | - |
| A1 | 0.02 | 0.02 | 0.02 | 0.02 | $+0.03 /-0.02$ | - |
| b | 0.25 | 0.25 | 0.23 | 0.22 | $\pm 0.02$ | - |
| c | 0.20 | 0.20 | 0.20 | 0.20 | Reference | - |
| D | 7.00 | 5.00 | 8.00 | 5.00 | Basic | - |
| D2 | 5.10 | 3.80 | 5.80 | $3.60 / 2.48$ | Reference | 8 |
| E | 7.00 | 7.00 | 8.00 | 6.00 | Basic | - |
| E2 | 5.10 | 5.80 | 5.80 | $4.60 / 3.40$ | Reference | 8 |
| e | 0.50 | 0.50 | 0.80 | 0.50 | Basic | - |
| L | 0.55 | 0.40 | 0.53 | 0.50 | $\pm 0.05$ | - |
| N | 44 | 38 | 32 | 32 | Reference | 4 |
| ND | 11 | 7 | 8 | 7 | Reference | 6 |
| NE | 11 | 12 | 8 | 9 | Reference | 5 |


|  | MILLIMETERS |  |  |  |  |  | TOLER- <br> SYMBOL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| QFN28 | QFN2 | QFN20 |  | QFN16 | NOTES |  |  |
| A | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | $\pm 0.10$ | - |
| A1 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 | $+0.03 /$ <br> -0.02 | - |
| b | 0.25 | 0.25 | 0.30 | 0.25 | 0.33 | $\pm 0.02$ | - |
| c | 0.20 | 0.20 | 0.20 | 0.20 | 0.20 | Reference | - |
| D | 4.00 | 4.00 | 5.00 | 4.00 | 4.00 | Basic | - |
| D2 | 2.65 | 2.80 | 3.70 | 2.70 | 2.40 | Reference | - |
| E | 5.00 | 5.00 | 5.00 | 4.00 | 4.00 | Basic | - |
| E2 | 3.65 | 3.80 | 3.70 | 2.70 | 2.40 | Reference | - |
| e | 0.50 | 0.50 | 0.65 | 0.50 | 0.65 | Basic | - |
| L | 0.40 | 0.40 | 0.40 | 0.40 | 0.60 | $\pm 0.05$ | - |
| N | 28 | 24 | 20 | 20 | 16 | Reference | 4 |
| ND | 6 | 5 | 5 | 5 | 4 | Reference | 6 |
| NE | 8 | 7 | 5 | 5 | 4 | Reference | 5 |

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NOTES:

1. Dimensioning and tolerancing per ASME Y14.5M-1994.
2. Tiebar view shown is a non-functional feature.
3. Bottom-side pin \#1 I.D. is a diepad chamfer as shown.
4. N is the total number of terminals on the device.
5. NE is the number of terminals on the " $E$ " side of the package (or Y-direction).
6. ND is the number of terminals on the " $D$ " side of the package (or X -direction). ND = (N/2)-NE.
7. Inward end of terminal may be square or circular in shape with radius (b/2) as shown.
8. If two values are listed, multiple exposed pad options are available. Refer to device-specific datasheet.
